

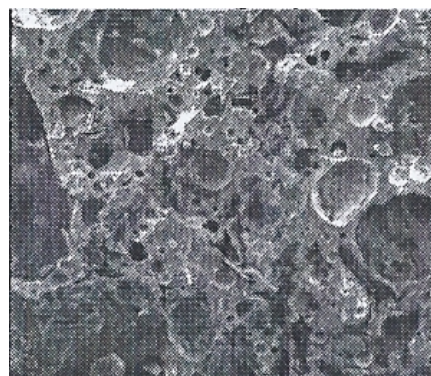
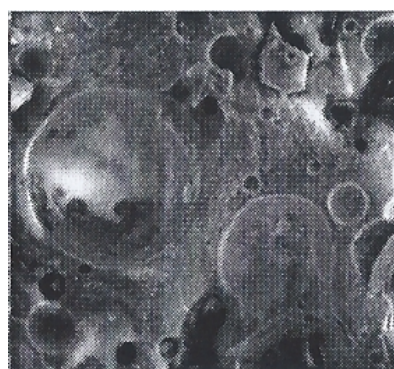
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(- ; -),

$$= 0,5, \quad V = 0,3 /$$

$$= 80 \quad 60 .$$



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$$(= 0,5, \quad V = 0,3 / , \quad = 80 ; \quad 100)$$

[3],

I

$$R_z = 0,8 - 1,25 :$$

$$I = 3,254 \begin{matrix} + \\ 0,867 \end{matrix} \begin{matrix} + \\ 1,012 \end{matrix} \begin{matrix} + \\ 0,535 \end{matrix} \begin{matrix} + \\ 0,118 \end{matrix} p^{0,692} V \begin{matrix} + \\ 0,461 \end{matrix} \begin{matrix} + \\ 0,225 \end{matrix}, \quad / ;$$

$$I = 2,942 \begin{matrix} + \\ 0,849 \end{matrix} \begin{matrix} + \\ 1,005 \end{matrix} \begin{matrix} + \\ 0,591 \end{matrix} \begin{matrix} + \\ 0,129 \end{matrix} p^{0,648} V \begin{matrix} + \\ 0,524 \end{matrix} \begin{matrix} + \\ 0,257 \end{matrix}, \quad / ;$$

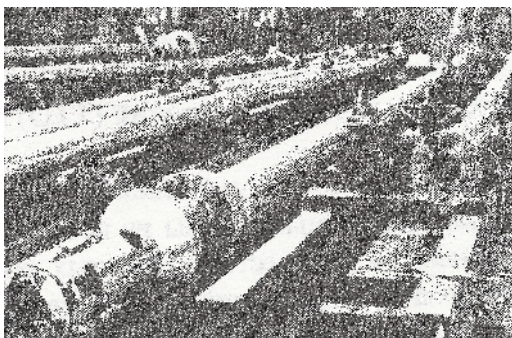
$$I = 3,013 \begin{matrix} + \\ 0,905 \end{matrix} \begin{matrix} + \\ 1,106 \end{matrix} \begin{matrix} + \\ 0,579 \end{matrix} \begin{matrix} + \\ 0,098 \end{matrix} p^{0,586} V \begin{matrix} + \\ 0,493 \end{matrix} \begin{matrix} + \\ 0,236 \end{matrix}, \quad / ;$$

$$I = 2,865 \begin{matrix} + \\ 1,109 \end{matrix} \begin{matrix} + \\ 1,205 \end{matrix} \begin{matrix} + \\ 0,472 \end{matrix} \begin{matrix} + \\ 0,274 \end{matrix} p^{0,563} V \begin{matrix} + \\ 0,465 \end{matrix} \begin{matrix} + \\ 0,348 \end{matrix}, \quad / ;$$

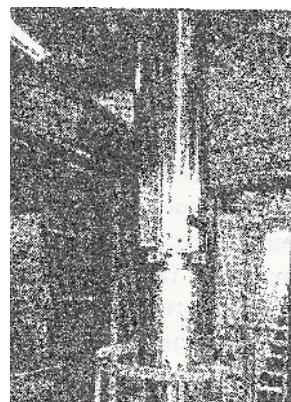
$$I = 2,754 \begin{matrix} + \\ 1,008 \end{matrix} \begin{matrix} + \\ 1,314 \end{matrix} \begin{matrix} + \\ 0,501 \end{matrix} \begin{matrix} + \\ 0,218 \end{matrix} p^{0,439} V \begin{matrix} + \\ 0,482 \end{matrix} \begin{matrix} + \\ 0,319 \end{matrix}, \quad / ;$$

$$I = 3,842 \begin{matrix} + \\ 1,105 \end{matrix} \begin{matrix} + \\ 1,143 \end{matrix} \begin{matrix} + \\ 0,492 \end{matrix} \begin{matrix} + \\ 0,196 \end{matrix} p^{0,573} V \begin{matrix} + \\ 0,504 \end{matrix} \begin{matrix} + \\ 0,418 \end{matrix}, \quad / ;$$

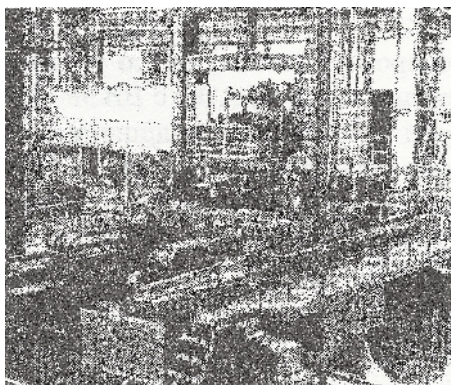
$I = 3,906^{1,132} p^{0,512} V^{0,216} p^{0,506} V^{0,478} 0,397$, / ,
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 $p -$, ;
 $V -$, / ;
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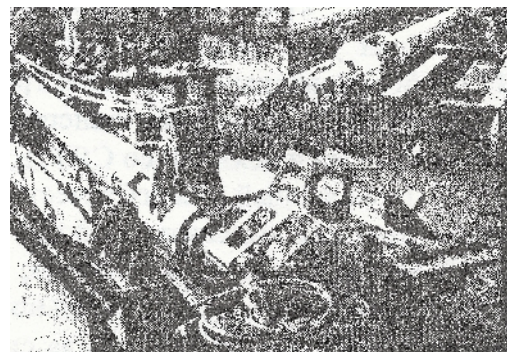
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621.9: 658.5

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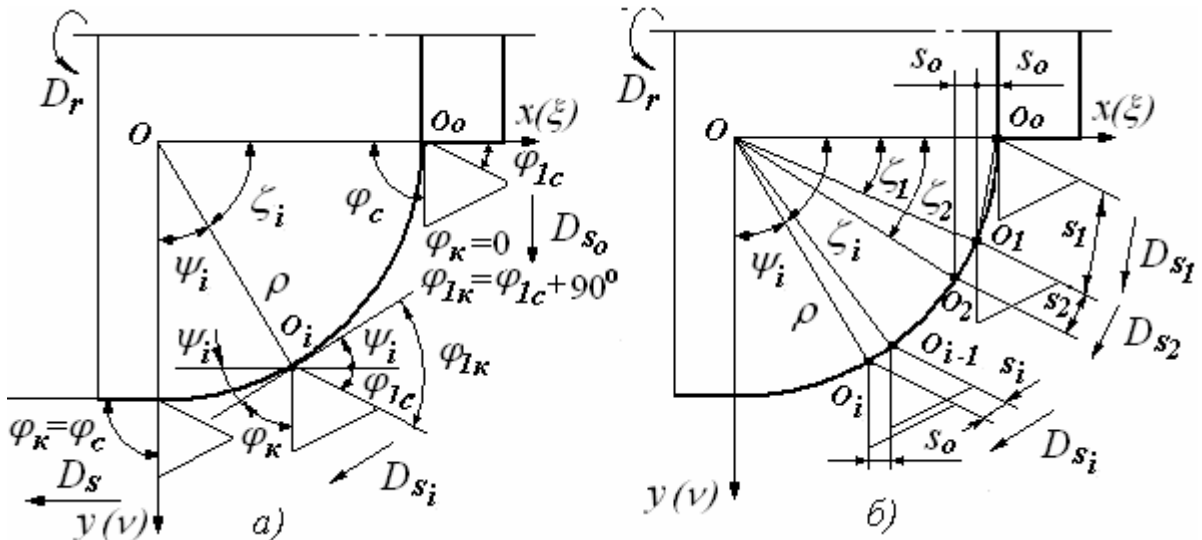
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 l s -
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).
 $\therefore \quad = 90^\circ ; \quad l = 30^\circ$ s .
 $= 90^\circ$ - , :

$$\cos \zeta_i = \sin \psi_i = (\rho - x) / \rho = 1 - \xi ; \quad \psi_i = \arcsin(1 - \xi), \quad (1)$$

$= x / \rho$ -

D_S : (. 1)

$$\varphi_K = \varphi_C - \psi_i = \varphi_C - \arcsin(1 - \xi); \quad \varphi_{1K} = \varphi_{1C} + \psi_i = \varphi_{1C} + \arcsin(1 - \xi). \quad (2)$$



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$$= 0, \quad l = 120^\circ .$$

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l (. 1)

$$s_l = l, \quad l = 1(1) \quad):$$

$$s_1(\xi) = O_o O_1 \approx \rho \zeta_1 = \rho \arccos((\rho - s_o) / \rho) = \rho \arccos(1 - \xi). \quad (3)$$

$$(-) \quad s = -l :$$

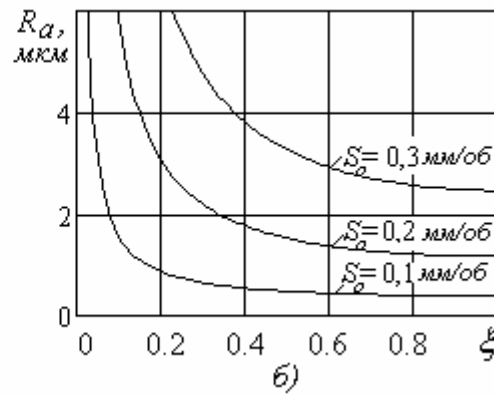
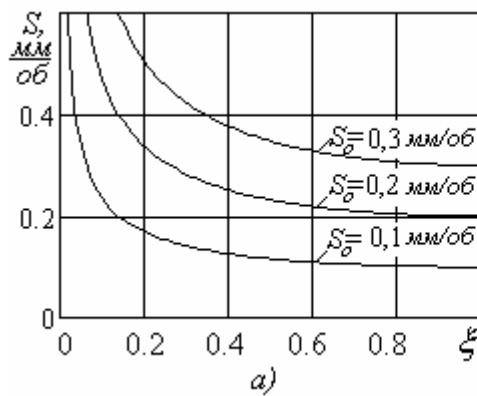
$$s_i(\xi) = O_{i-1}O_i \approx \rho(\zeta_i - \zeta_{i-1}) = \rho[\arccos(1-i\xi) - \arccos(1-(i-1)\xi)]. \quad (5)$$

R -

$$R_z; R = 0,005R_z [1]:$$

$$R_z(\xi) = \begin{cases} \frac{r}{\cos \gamma} - \frac{\sqrt{4r^2 - s(\xi)^2}}{2\cos \gamma} + \frac{b_c(2s(\xi) + b_c)}{32r} + R_u, & \varphi_{1K} \geq \arcsin \frac{s_i(\xi)}{2r} \leq \varphi_K; \\ \frac{b_c}{1/\tan \varphi_K + 2r/s(\xi)} + \frac{r(1 - \cos \varphi_K)}{\cos \gamma} + R_u + \\ + \frac{\sin \varphi_K \left[s(\xi) \cos \varphi_K - \sqrt{s(\xi) \sin \varphi_K (2r - s(\xi) \sin \varphi_K)} \right]}{\cos \gamma}, & \varphi_{1K} < \arcsin \frac{s_i(\xi)}{2r} \leq \varphi_K, \end{cases}$$

r - ; b - ; R - ; $b_c = 0,5\rho(1-2\tau_0/\sigma)$; ρ - ; σ, τ_0 -



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621.713

[illegible]

Abstract: In the paper attempted to systematize the structures of iron and steel grade designations in the system of the standards GOST in the image of European standards (EN 10027-1:2005).

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			()	1, 2, 3 (- %Si)	
			()		
(1, 2, 3, 4, 5, 6, P1, P2, P3, P4, P5, P6, P7)			(-)	1...6 (- %Si)	
			()	1...7 (- %Si)	
(10, 15, 20, 30, 35)				nn (daN/mm ²) ,	
(30-6, 50-5, 65-3, 70-2)				nn-mm (/ ² , , %)	
(35, 70, 90)				nn (/ ²) ,	
			()		
(-1, -1, -1, -2)				()	1, 2 ()
				()	1...6 ()
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 ✓ : () () - 1, 2;
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- $nn -$ () / ²
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(235, C345 , 590)		C (-)	nnn (/ ²)	() ()	()	
(10 , 35, 45 , 58A)			nn (%)		(- -)	
(12XH3, 30XH2B)			nn (%)	EaEaEa (: E %)	(- -)	
(12 13, 17X18H9)				Xa_xEaEa (: E %, - a_x)		
(110 13 , 30 10 10)				EaEaEa (: E %)		
(65, 60 2)					()	
(10 14 14 4)						
(45, 15 , 12 8)						
(18 , 12 1)			nn (%)	K () EaEaEa (: E %)		
(20, 40, 38)	A	AC (-)	nn (%)			
				EaEaEa (: E)		

. 2.

1	2	3	4	5	6	7
(15, 20 , 8 4 9 2-)		(-)		a_xEE (% a_x,)		
			nn (%)	Xa_xEaEa (: %, E - a_x)	()	
(9, 11A, 8)		(-)	nn (%)	EaEaEa (: E %)	(-)	
(, 3 2)						
(6 5 3, 11 3 3 2)				PaMa aKa (: E % W (P B), Mo (M), V (), Co (K)		
			nn (%)			

- **nn** **nnn** - 2 3 (, ,);
- , - (0,2%);
- **K** ();
- **EaEaEa** - (: (), (), (), (), (), () . ;
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➤ : (P B - (M), (), (K) (**PaMa aKa**);
➤ ;
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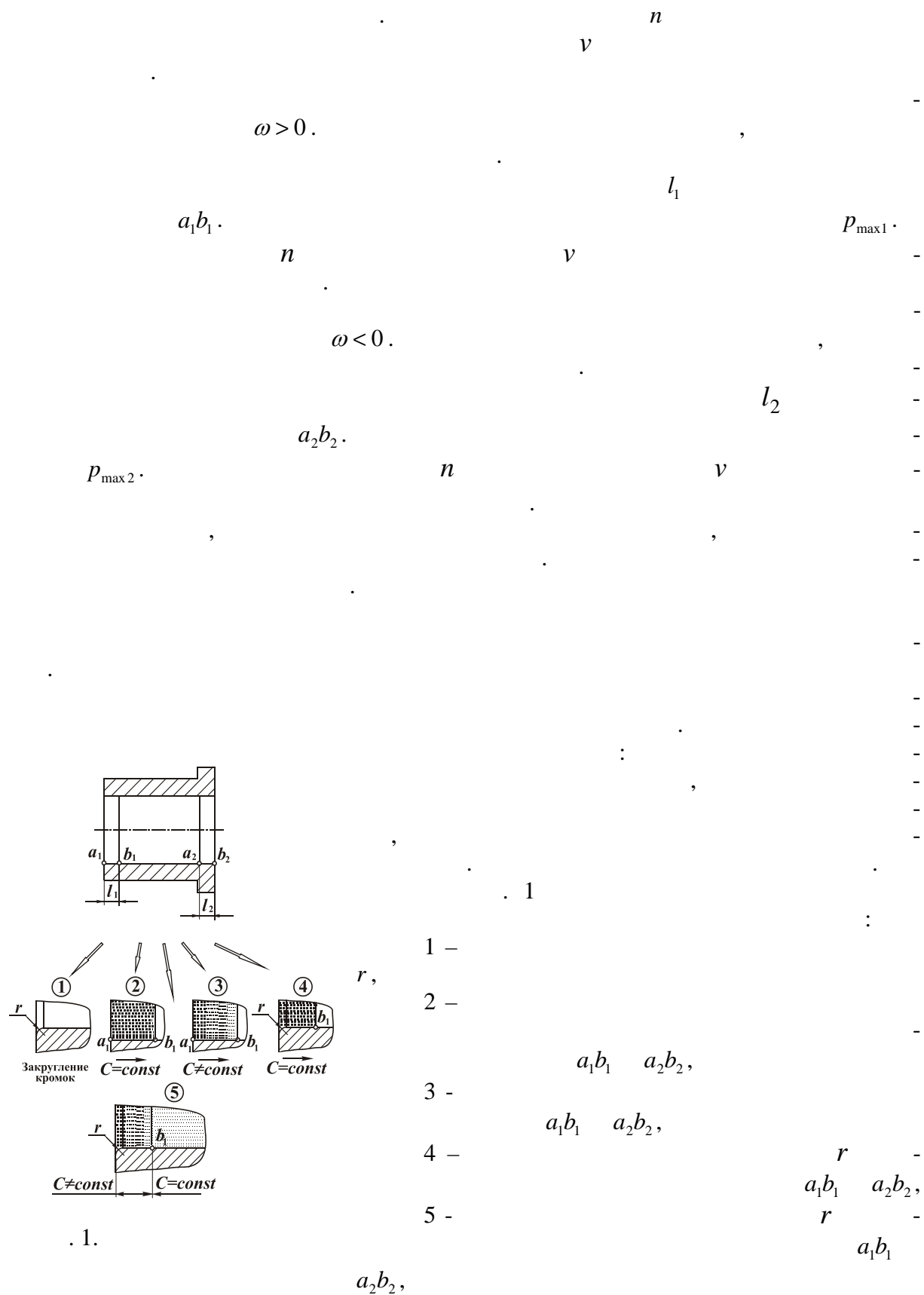
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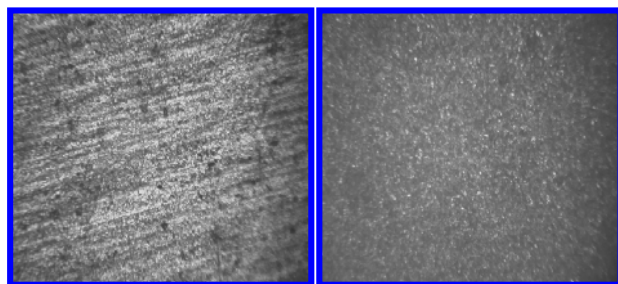
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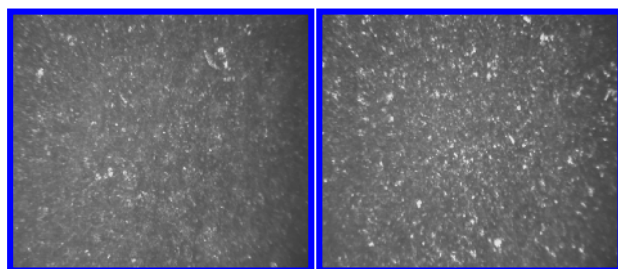
$$(l - l_1 - l_2).$$

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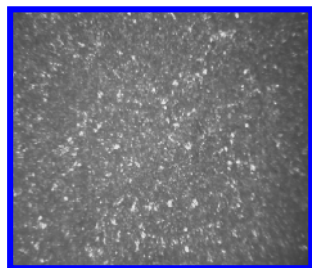


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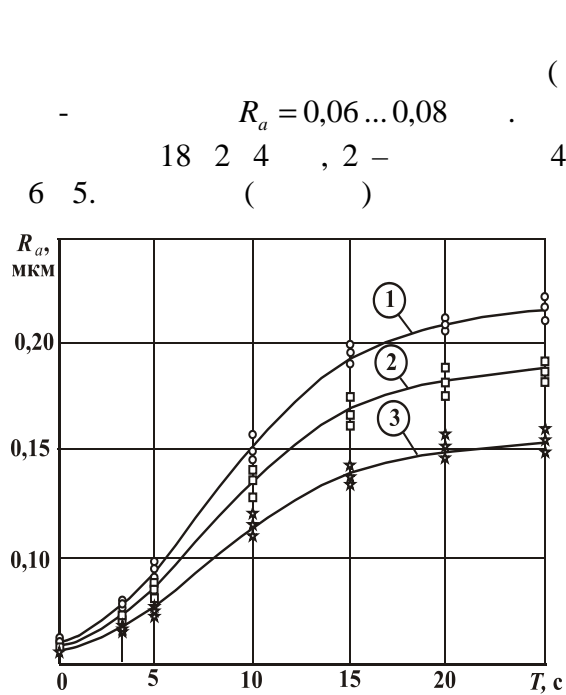


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 6 5. () :
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 25 – 30 %.

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 2006. . 32 – 35.