

Solution of the problem 10.9

Computation of the transient process while an iron core coil is switched on direct current source by method of graphical integration

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ORIGIN := 1      Magnetization curve of steel 1512
BH1 := (0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1 1.1)
        (0 0.13 0.25 0.35 0.5 0.65 0.8 0.95 1.15 1.5 2.0 3.0)
BH2 := (1.15 1.2 1.25 1.3 1.35 1.4 1.45 1.5 1.55 1.6 1.7 1.76)
        (3.7 4.65 6 7.2 9.2 12 15 23 33 49 90 120)
BH := augment(BH1, BH2)      Bi := (BH^T)^(1)      Hi := (BH^T)^(2)
J := 10      R := 1      l := 50      w := 490      S := 10^-2

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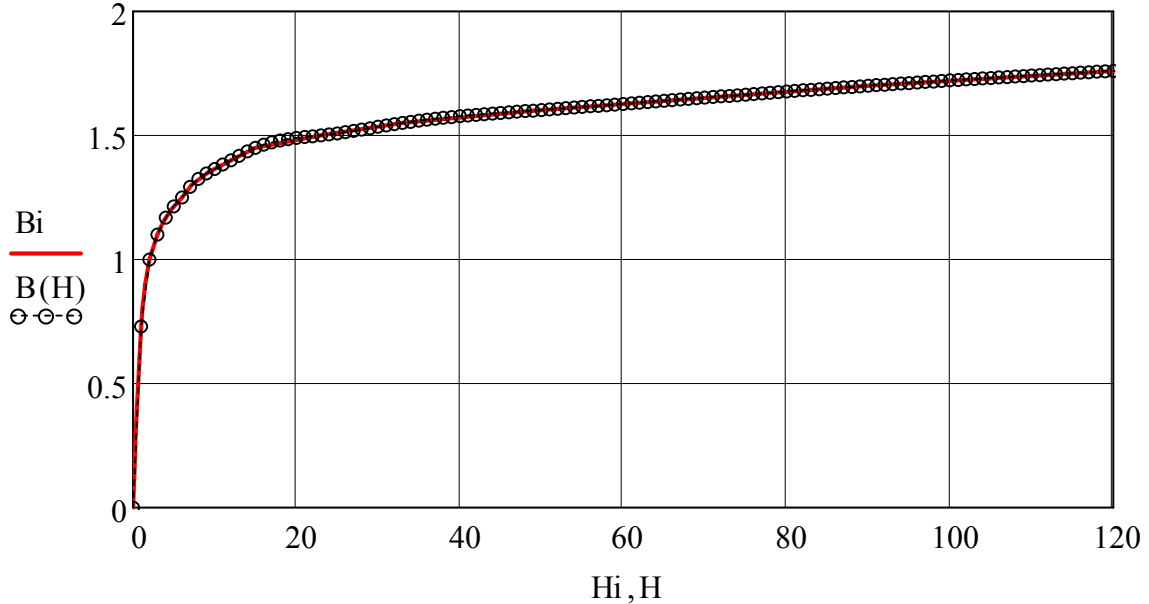
Spline-approximation of dependence B(H)

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vHB := lspline(Hi, Bi)      fB(x) := interp(vHB, Hi, Bi, x)      length(Bi) = 24
vBH := lspline(Bi, Hi)      fH(x) := interp(vBH, Bi, Hi, x)
B(H) := fB(H)      H := 0, 1 .. 120

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Verification of the approximation



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Steady-state values of current, magnetic intensity and induction      Number of
                                                                           integration points
Iu := J      Hu := (w * Iu) / l      Bu := fB(Hu)      m := 200
Iu = 10      Hu = 98      Bu = 1.717      Bm := 0.995 * Bu      i := 1 .. m
Integration step      dB := (Bm) / m      dPsi := dB * w * S

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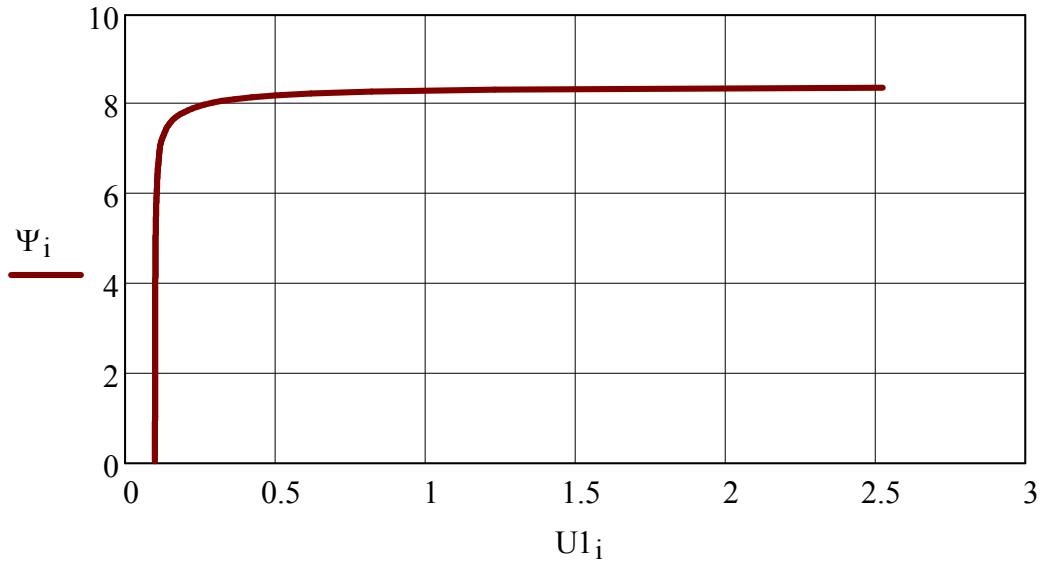
Verification

$$\Psi_i := i \cdot \text{dB} \cdot w \cdot S$$

$$I_i := \frac{1 \cdot fH(i \cdot \text{dB})}{w}$$

Function to integrate

$$U1_i := \frac{1}{(J - I_i) \cdot R}$$



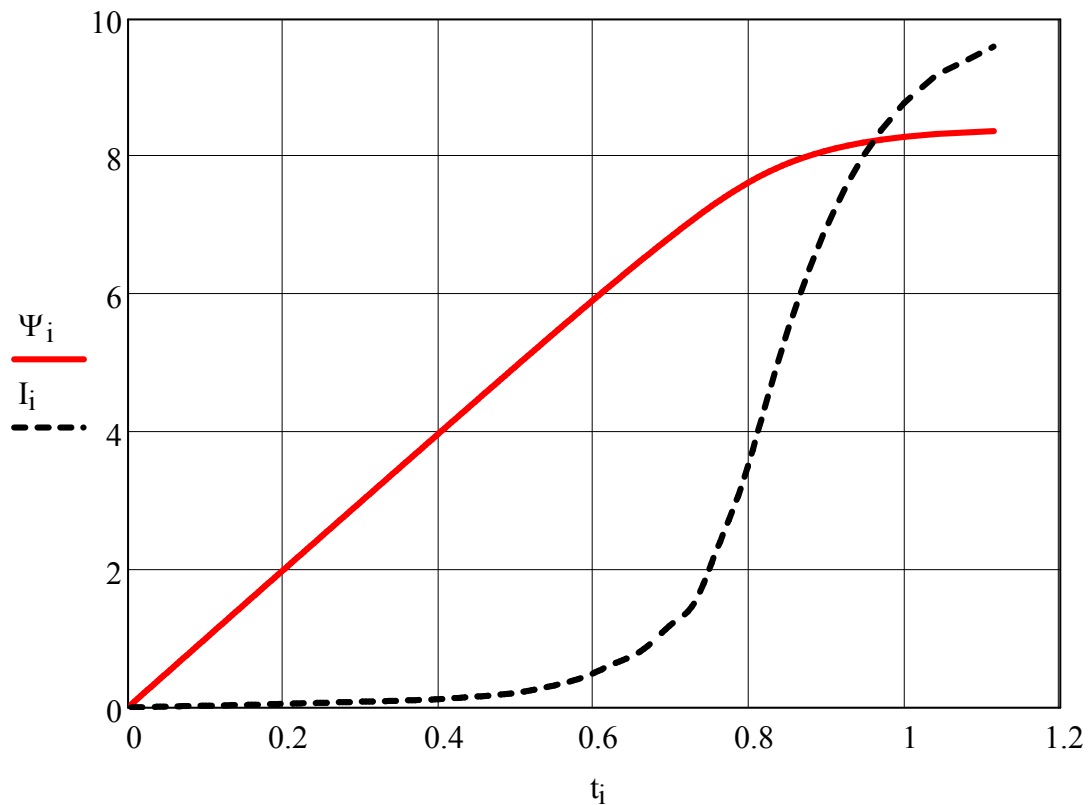
Dependences $\Psi(t)$ and $i(t)$ and their graphs

$$k := 1 .. m \quad t_k := k \cdot d\Psi \quad \underline{s} := \text{cspline}(t, U1)$$

$$\underline{g} := 1, 2 .. m$$

$$t_i := T(i)$$

$$\underline{T}(g) := \int_0^{g \cdot d\Psi} \text{interp}(s, t, U1, x) dx$$



solution of the problem 1 0.1 0

Computation of the transient process while an iron core coil is switched on sinusoidal voltage

Magnetization curve

ORIGIN := 1

$$BT1 := (0 \ .1 \ .2 \ .3 \ .4 \ .5 \ .6 \ .7 \ .8 \ .9 \ 1 \ 1.1 \ 1.15)$$

$$BT2 := (1.2 \ 1.25 \ 1.3 \ 1.35 \ 1.4 \ 1.45 \ 1.5 \ 1.55 \ 1.6 \ 1.7 \ 1.76)$$

$$HT1 := (0 \ 18 \ 25 \ 35 \ 50 \ 65 \ 80 \ 95 \ 115 \ 150 \ 200 \ 300 \ 370)$$

$$HT2 := (465 \ 600 \ 740 \ 900 \ 1200 \ 1500 \ 2200 \ 3300 \ 4900 \ 9000 \ 12000)$$

$$BT := \text{augment}(BT1, BT2) \quad HT := \text{augment}(HT1, HT2)$$

$$H := HT^T \quad B := BT^T \quad U := 2000 \quad R := 2 \quad l := 0.5 \quad w := 200 \quad S := 2 \cdot 10^{-2}$$

$$\Psi := B \cdot S \cdot w \quad I := \frac{H \cdot l}{w} \quad \text{Approximation of dependence } \Psi(I) \quad m := \text{length}(B)$$

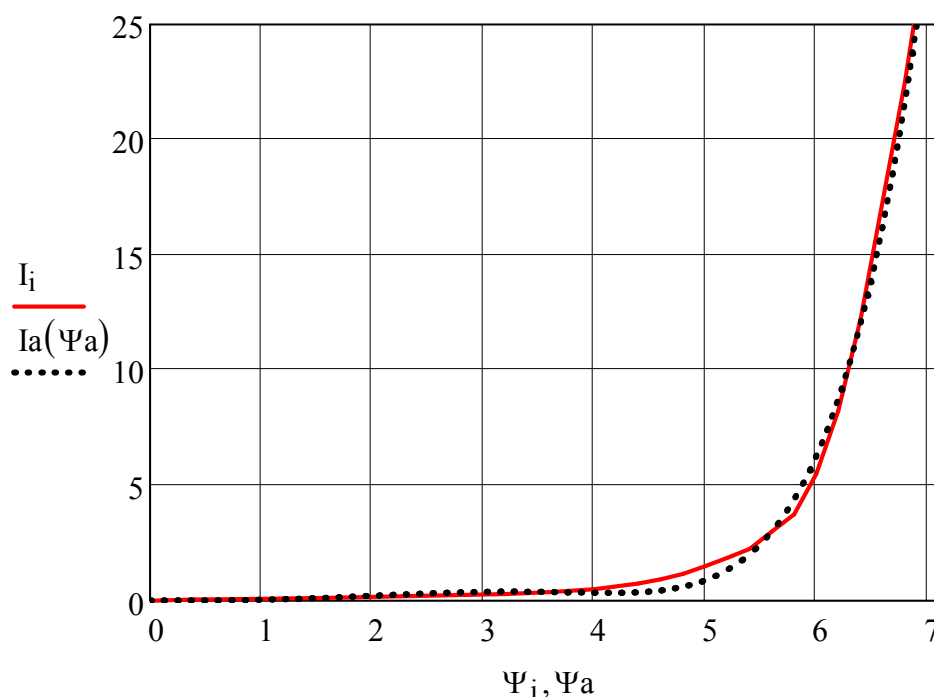
$$Ik := \begin{bmatrix} \Psi_5 & (\Psi_5)^3 & (\Psi_5)^5 & (\Psi_5)^7 \\ \Psi_{10} & (\Psi_{10})^3 & (\Psi_{10})^5 & (\Psi_{10})^7 \\ \Psi_{18} & (\Psi_{18})^3 & (\Psi_{18})^5 & (\Psi_{18})^7 \\ \Psi_{24} & (\Psi_{24})^3 & (\Psi_{24})^5 & (\Psi_{24})^7 \end{bmatrix} \quad \Psi_k := \begin{pmatrix} I_5 \\ I_{10} \\ I_{18} \\ I_{24} \end{pmatrix} \quad \Psi_k = \begin{pmatrix} 0.125 \\ 0.375 \\ 3 \\ 30 \end{pmatrix}$$

$$K := Ik^{-1} \cdot \Psi_k$$

Verification

$$Ia(\Psi a) := K_1 \cdot \Psi a + K_2 \cdot \Psi a^3 + K_3 \cdot \Psi a^5 + K_4 \cdot \Psi a^7 \quad i := 0, 1 .. m$$

$$\Psi_{24} = 7.04$$



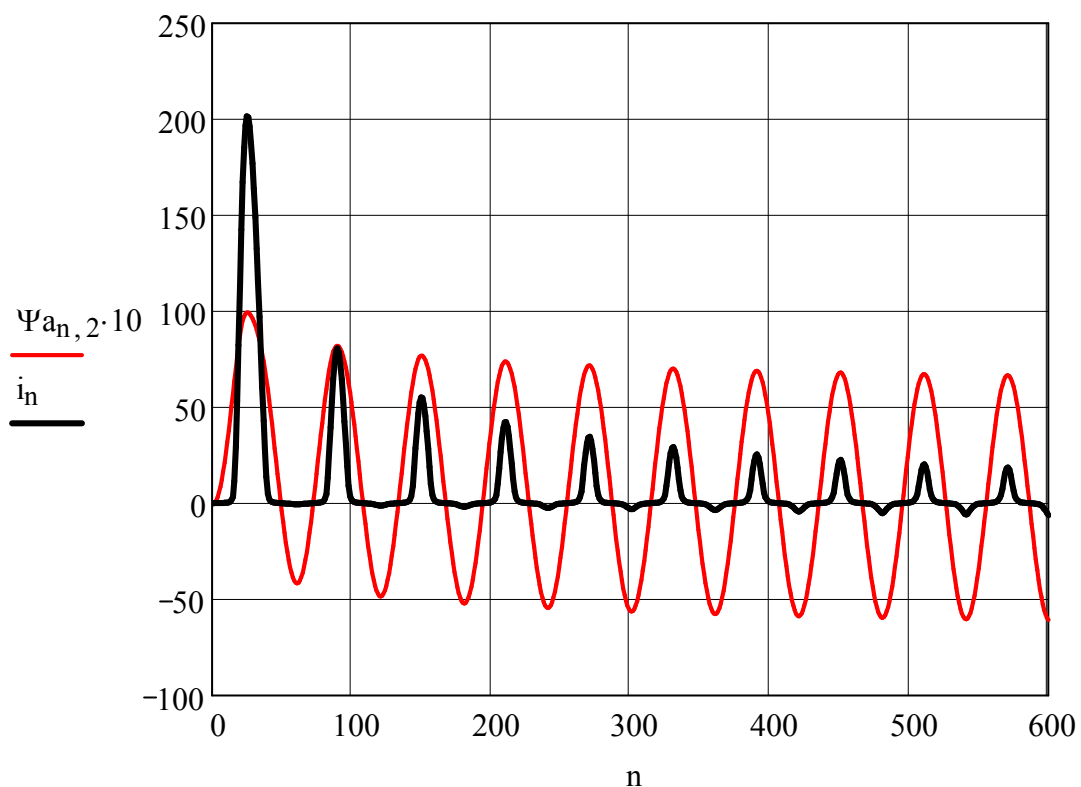
$p := 0$ Solution of the differential equation by Runge-Kutt method

$$U_r(t, p) := U \cdot \sin(100 \cdot \pi \cdot t) - R \cdot (K_1 \cdot p + K_2 \cdot p^3 + K_3 \cdot p^5 + K_4 \cdot p^7)$$

$$\Psi_a := \text{Rkadapt}(p, 0, 0.2, 600, U_r) \quad n := 1 \dots 600$$

Interpolation of $\Psi(I)$ $\text{vbh} := \text{pspline}(\Psi, I)$ $\text{fh}(x) := \text{interp}(\text{vbh}, \Psi, I, x)$

$$\text{Current determination} \quad i_n := \begin{cases} \text{fh}(\Psi_{a_n, 2}) & \text{if } \Psi_{a_n, 2} > 0 \\ -\text{fh}(|\Psi_{a_n, 2}|) & \text{otherwise} \end{cases}$$



Determination of the approximate values of amplitudes of the current and flux-linkage in steady-state condition

$$\Psi_u := \frac{U}{100 \cdot \pi} \quad \Psi_u = 6.366 \quad \underline{I_u} := \text{fh}(\Psi_u) \quad I_u = 11.505$$

$$\frac{\max(i)}{I_u} = 17.511$$